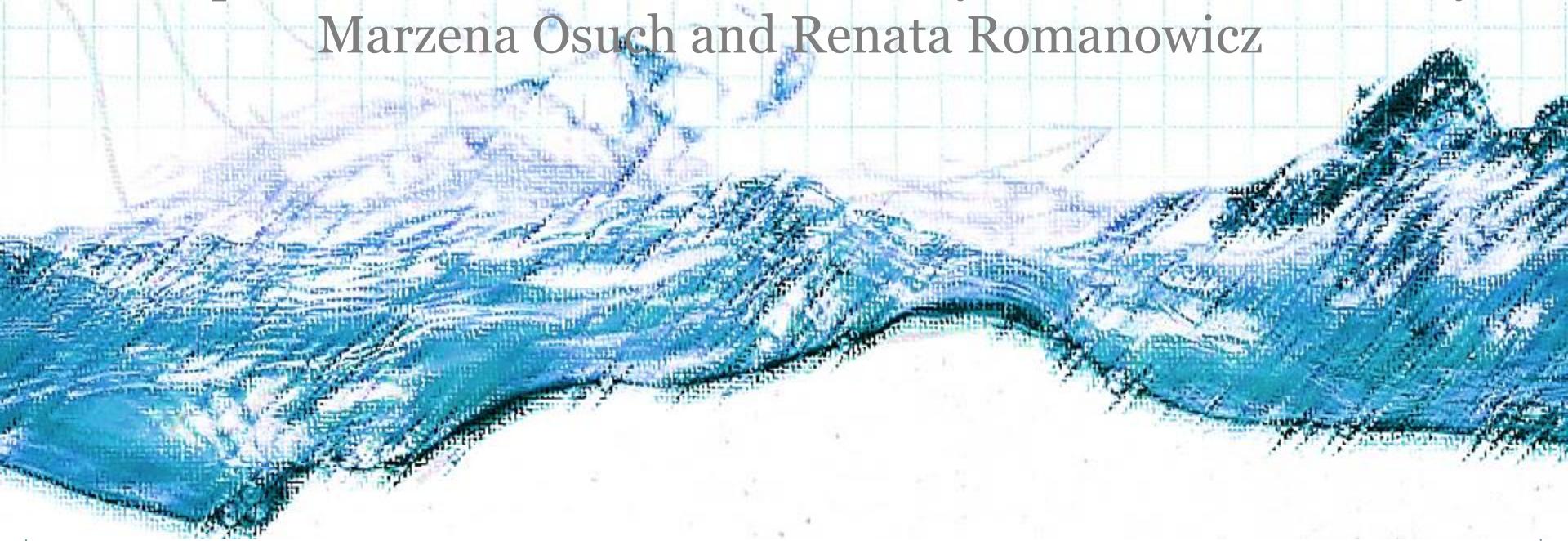




CLIMATE CHANGE IMPACT ON HYDROLOGICAL EXTREMES

The influence of HBV model parameters nonstationarity on flow predictions for future climate; Nysa Kłodzka case study

Marzena Osuch and Renata Romanowicz



Supported by a grant from the Norwegian Financial Mechanism



Institute of Geophysics
Polish Academy of Sciences

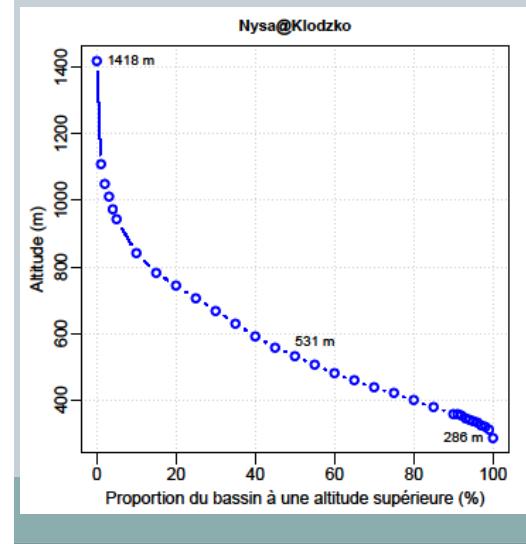
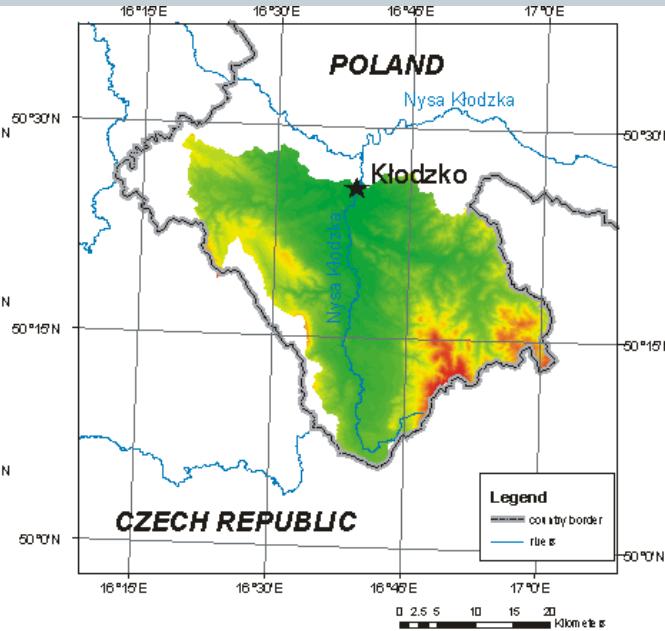


Norwegian Water Resources
and Energy Directorate

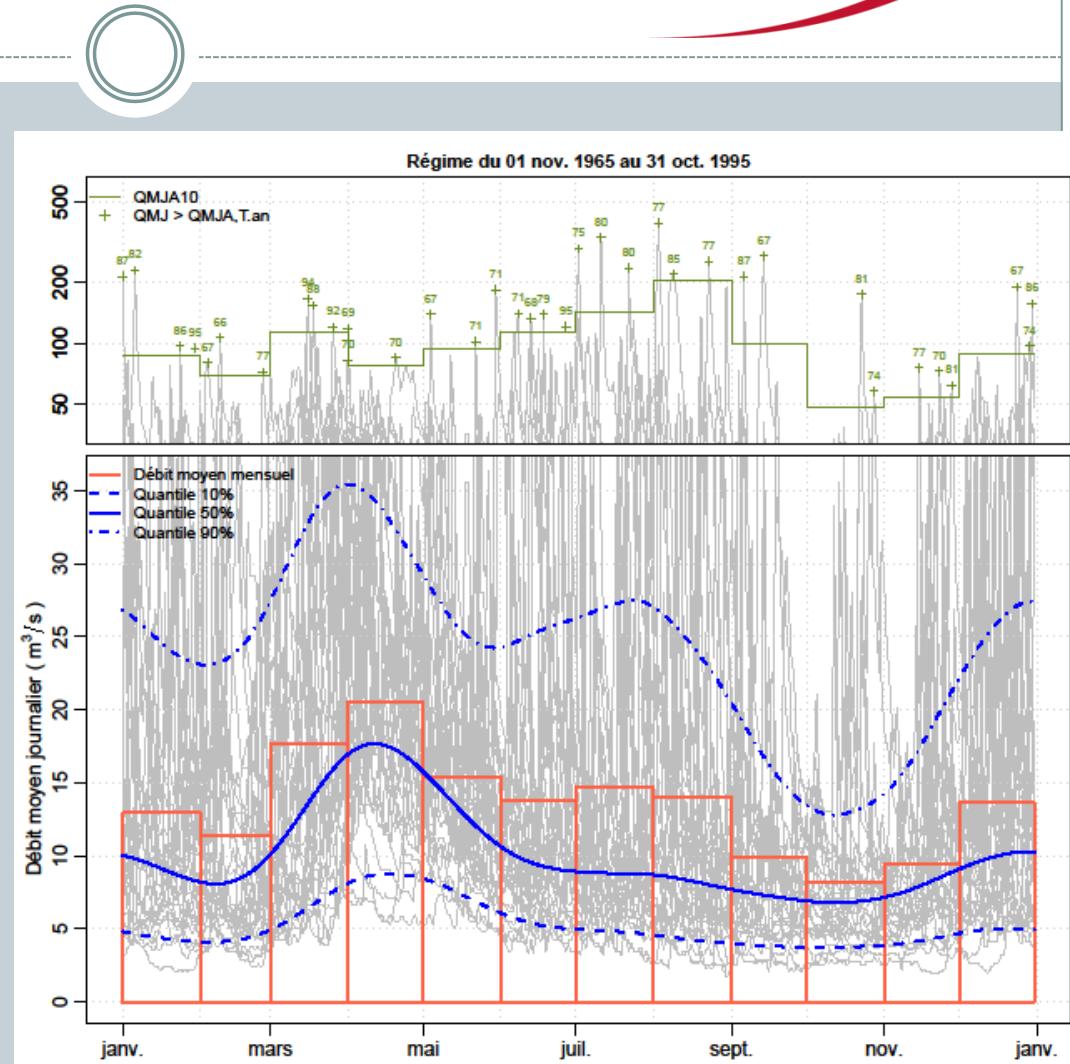


- Case study – Nysa Kłodzka
- Methodology
 - Calibration and validation HBV model
 - Sensitivity analysis - Model simplification
 - Regression models - Dependence of model parameters on climate characteristics
 - Flow and flood quantiles predictions in future climate
- Results
- Conclusions

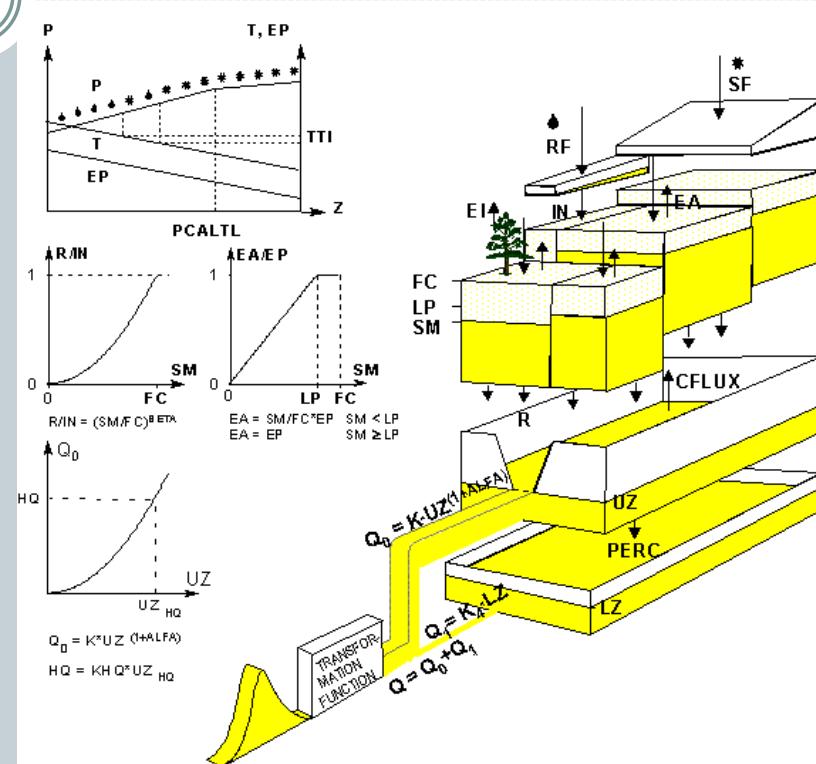
- Located in southern part of Poland
- Catchment area 1083 km² up to Kłodzko gauging station
- Typical mountainous catchment with a bottom slope about 1%, zmin=286, z50=531, zmax=1418
- This catchment has been affected by several devastating floods e.g. in 1967, 1975, 1977, 1980, 1982, 1985, 1997, 1998, 2006 and 2009.



- Available data from 01/11/1965 to 31/10/2010
- Flow regime - mixed
 - Spring floods due to snowmelt
 - Summer floods due to convective rainfall
- Natural flow conditions without significant changes in land use and water management



- Nordic version of HBV model
- Conceptual lumped rainfall-runoff model with 15 parameters
- Inputs: precipitation, air temperature and discharges at daily time step
- Optimization method – DEGL Differential Evolution with Global and Local neighbours
- Problems with calibration for long time series
- Model calibration for five consecutive year periods, moving window



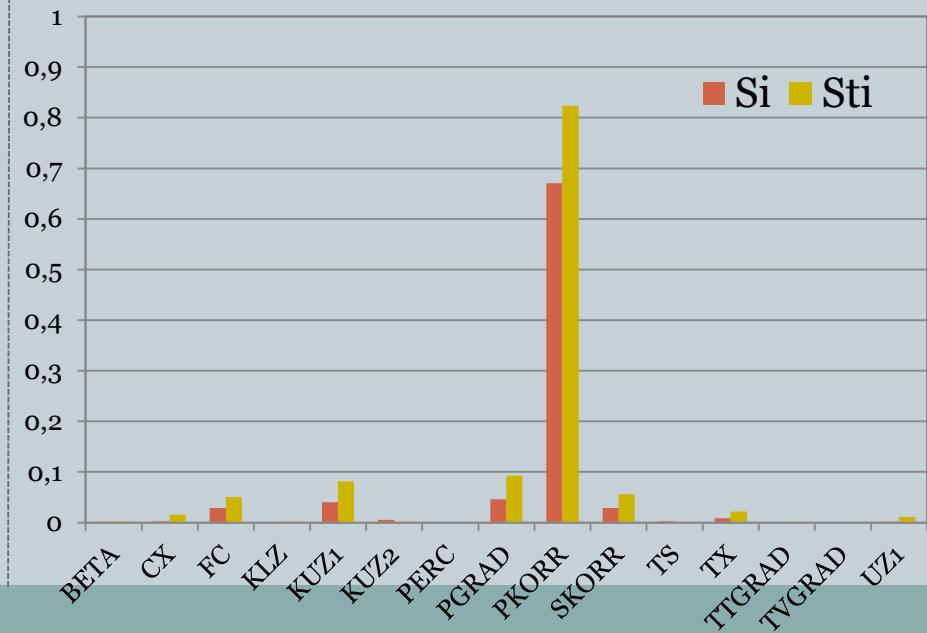
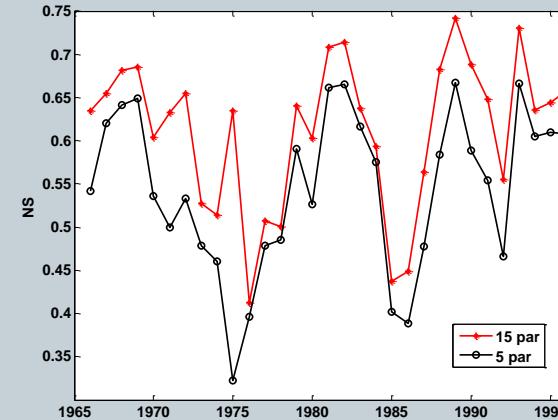
P = Precipitation
 T = Temperature
 SF = Snow
 RF = Rain
 Z = Elevation
 PCALTL = Threshold for altitude correction
 TTI = Threshold temperature interval
 IN = Infiltration
 EP = Potential evapotranspiration
 EA = Actual evapotranspiration
 EI = Evaporation from interception
 SM = Soil moisture storage
 FC = Maximum soil moisture storage
 LP = Limit for potential evapotranspiration

BETTA = Soil parameter
 R = Recharge
 CFLUX = Capillary transport
 UZ = Storage in upper response box
 LZ = Storage in lower response box
 PERC = Percolation
 K, K_4 = Recession parameters
 ALFA = Recession parameter
 Q_0, Q_1 = Runoff components
 HQ = High flow parameter
 KHQ = Recession at HQ
 HQ_{UZ} = UZ level at HQ

- Results of optimization – 5 year period
- Nash Sutcliffe criterion –three periods with NS>0.7 validation

	1966	1967	1968	1969	1970	1971	1972	1973	1974	1975	1976	1977	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	
1966	0.63	0.53	0.44	0.53	0.21	-0.04	0.28	0.04	0.21	0.63	0.40	0.43	0.49	0.04	0.14	0.46	0.33	0.49	0.45	0.30	0.34	-0.44	0.16	0.28	0.13	-0.20	0.04	-0.49	0.14	0.16	-0.66	
1967	0.59	0.65	0.63	0.64	0.33	-0.05	0.26	0.01	0.20	0.59	0.47	0.49	0.57	0.00	0.11	0.48	0.46	0.47	0.43	0.27	0.26	-0.56	0.07	0.22	0.13	-0.29	-0.07	-0.58	0.05	0.06	-0.91	
1968	0.47	0.65	0.68	0.66	0.35	-0.05	0.13	-0.10	0.11	0.47	0.49	0.47	0.56	NaN	-0.05	0.47	0.47	0.42	0.37	0.16	0.08	-0.85	-0.14	0.05	0.04	-0.47	-0.16	-0.67	-0.09	-0.04	-1.12	
1969	0.50	0.64	0.66	0.69	0.39	0.00	0.15	-0.10	0.14	0.50	0.48	0.50	0.57	NaN	NaN	0.47	0.48	0.44	0.42	0.21	0.16	-0.73	-0.05	0.13	0.07	-0.38	-0.11	-0.60	-0.08	-0.04	-1.05	
1970	0.39	0.51	0.51	0.56	0.60	0.49	0.41	0.41	0.42	0.39	0.51	0.51	0.52	0.27	0.34	0.43	0.45	0.40	0.38	0.39	0.29	0.15	0.30	0.36	0.34	0.25	0.22	0.29	0.33	0.32	0.10	
1971	0.39	0.35	0.37	0.41	0.57	0.63	0.52	0.51	0.54	0.39	0.47	0.44	0.46	0.37	0.41	0.40	0.36	0.43	0.40	0.41	0.33	0.20	0.34	0.36	0.31	0.38	0.44	0.52	0.48	0.49	0.44	
1972	0.46	0.40	0.37	0.44	0.51	0.56	0.66	0.61	0.62	0.46	0.48	0.47	0.51	NaN	NaN	0.46	0.37	0.45	0.42	0.42	0.38	0.21	0.43	0.44	0.38	0.44	0.46	0.43	0.54	0.54	0.45	
1973	0.38	0.31	0.29	0.31	0.37	0.42	0.52	0.53	0.52	0.38	0.39	0.35	0.40	0.44	0.39	0.32	0.28	0.34	0.30	0.29	0.30	0.18	0.33	0.34	0.25	0.33	0.38	0.37	0.44	0.44	0.35	
1974	0.36	0.31	0.30	0.31	0.38	0.43	0.49	0.50	0.51	0.36	0.39	0.35	0.37	0.42	0.38	0.31	0.28	0.33	0.30	0.27	0.27	0.15	0.30	0.30	0.23	0.31	0.36	0.36	0.40	0.43	0.32	
1975	0.23	0.26	0.24	0.23	0.08	-0.18	0.06	-0.12	0.03	0.23	0.29	0.27	0.25	-0.23	-0.08	0.21	0.20	0.09	0.06	-0.07	-0.02	-0.45	-0.12	-0.04	-0.05	-0.15	-0.12	-0.54	-0.20	-0.07	-0.65	
1976	0.34	0.32	0.30	0.30	0.27	0.08	0.24	0.15	0.21	0.34	0.41	0.39	0.37	0.10	0.12	0.26	0.25	0.23	0.20	0.12	0.13	-0.17	0.12	0.15	0.01	0.05	0.13	-0.07	0.11	0.18	-0.21	
1977	0.37	0.40	0.37	0.37	0.33	0.03	0.20	0.05	0.12	0.37	0.48	0.51	0.45	0.03	0.09	0.34	0.35	0.27	0.23	0.14	0.07	-0.34	0.02	0.09	-0.03	-0.07	0.01	-0.20	0.04	0.13	0.25	
1978	0.40	0.41	0.36	0.37	0.38	0.18	0.26	0.10	0.23	0.40	0.48	0.50	0.50	NaN	NaN	0.40	0.39	0.34	0.31	0.24	0.17	-0.15	0.15	0.20	0.11	0.06	0.12	-0.01	0.15	0.21	-0.33	
1979	0.49	0.46	0.39	0.42	0.44	0.31	0.50	0.44	0.42	0.49	0.49	0.52	0.54	0.64	0.57	0.48	0.45	0.46	0.44	0.42	0.39	0.28	0.44	0.45	0.34	0.33	0.35	0.39	0.43	0.42	0.19	
1980	0.49	0.42	0.30	0.36	0.28	0.09	0.38	0.19	0.26	0.49	0.31	0.40	0.46	NaN	NaN	0.60	0.54	0.48	0.41	0.42	0.37	0.39	0.26	0.32	0.37	0.47	0.20	0.12	0.10	0.19	0.19	-0.20
1981	0.60	0.56	0.45	0.53	0.41	0.08	0.30	-0.08	0.20	0.60	0.47	0.51	0.57	0.14	0.45	0.71	0.63	0.58	0.59	0.44	0.46	0.33	0.42	0.44	0.57	0.37	0.37	-0.32	-0.38	-0.24	-0.46	
1982	0.55	0.60	0.50	0.58	0.47	0.06	0.26	-0.10	0.21	0.55	0.51	0.55	0.57	-0.02	0.36	0.69	0.71	0.63	0.61	0.47	0.37	0.25	0.30	0.37	0.50	0.33	0.34	-0.34	-0.53	-0.32	-0.63	
1983	0.53	0.53	0.44	0.51	0.50	0.38	0.38	0.21	0.37	0.53	0.49	0.52	0.54	0.12	0.34	0.57	0.58	0.64	0.62	0.54	0.41	0.32	0.39	0.44	0.46	0.45	0.49	0.09	-0.02	0.11	-0.08	
1984	0.48	0.44	0.35	0.43	0.44	0.35	0.33	0.14	0.31	0.48	0.44	0.48	0.47	0.11	0.32	0.52	0.49	0.58	0.59	0.53	0.42	0.36	0.38	0.42	0.44	0.42	0.42	0.06	-0.01	0.10	-0.04	
1985	0.30	0.23	0.11	0.23	0.26	0.30	0.27	0.21	0.24	0.30	0.22	0.28	0.25	0.27	0.28	0.27	0.24	0.39	0.40	0.44	0.36	0.33	0.31	0.34	0.30	0.29	0.23	0.31	0.29	0.32	0.25	
1986	0.34	0.18	0.05	0.17	0.21	0.27	0.25	0.19	0.22	0.33	0.18	0.23	0.18	0.32	0.28	0.23	0.19	0.35	0.34	0.42	0.45	0.40	0.40	0.38	0.26	0.24	0.15	0.29	0.26	0.28	0.20	
1987	0.34	0.12	-0.08	0.14	0.18	0.26	0.24	0.08	0.17	0.34	0.14	0.21	0.15	0.23	0.27	0.25	0.14	0.36	0.33	0.49	0.54	0.56	0.47	0.44	0.31	0.26	0.17	0.24	0.20	0.24	0.25	
1988	0.54	0.35	0.23	0.39	0.28	0.13	0.44	-0.01	0.39	0.54	0.34	0.33	0.42	0.35	0.49	0.36	0.54	0.43	0.52	0.56	0.42	0.47	0.44	0.31	0.49	0.28	0.00	0.30	0.36	-0.18		
1989	0.62	0.42	0.31	0.45	0.39	0.25	0.51	0.06	0.47	0.62	0.38	0.41	0.54	0.44	0.49	0.63	0.50	0.63	0.54	0.61	0.60	0.44	0.74	0.74	0.68	0.62	0.42	0.13	0.39	0.44	-0.01	
1990	0.29	0.32	0.29	0.37	0.41	0.30	0.38	0.02	0.33	0.29	0.36	0.40	0.51	NaN	NaN	0.56	0.36	0.55	0.52	0.56	0.41	0.37	0.51	0.55	0.69	0.66	0.48	0.19	0.32	0.39	0.13	
1991	0.30	0.31	0.29	0.38	0.41	0.34	0.37	0.09	0.35	0.30	0.37	0.40	0.48	0.28	0.36	0.48	0.33	0.54	0.52	0.52	0.57	0.37	0.34	0.49	0.53	0.60	0.65	0.50	0.27	0.36	0.41	0.21
1992	0.29	0.33	0.30	0.34	0.42	0.34	0.32	0.25	0.29	0.29	0.36	0.40	0.43	0.25	0.25	0.37	0.30	0.39	0.36	0.31	0.20	-0.35	0.27	0.34	0.27	0.45	0.56	0.47	0.41	0.46	0.38	
1993	0.34	0.37	0.38	0.38	0.62	0.65	0.56	0.59	0.56	0.34	0.53	0.57	0.51	0.58	0.53	0.39	0.42	0.48	0.49	0.38	0.27	0.26	0.35	0.33	0.33	0.35	0.56	0.73	0.69	0.70	0.66	
1994	0.35	0.36	0.38	0.37	0.57	0.57	0.54	0.56	0.52	0.35	0.51	0.52	0.49	NaN	NaN	0.39	0.41	0.45	0.45	0.33	0.25	0.22	0.32	0.30	0.31	0.51	0.61	0.64	0.64	0.61		
1995	0.36	0.37	0.39	0.38	0.57	0.58	0.53	0.55	0.51	0.36	0.51	0.53	0.50	0.57	0.54	0.40	0.43	0.46	0.47	0.35	0.27	0.24	0.34	0.32	0.32	0.52	0.62	0.64	0.64	0.62		
1996	0.35	0.35	0.37	0.37	0.58	0.60	0.54	0.56	0.51	0.35	0.51	0.53	0.49	NaN	NaN	0.41	0.43	0.48	0.49	0.39	0.32	0.40	0.37	0.35	0.38	0.56	0.52	0.62	0.64	0.64		

- Sensitivity analysis by Sobol method
- 5 parameters with significant influence on NS value
 - FC – field capacity (soil zone)
 - KUZ1 – recession constant (upper zone 1)
 - PGRAD – precipitation lapse rate
 - PKORR – rainfall correction factor
 - SKORR – snowfall correction factor

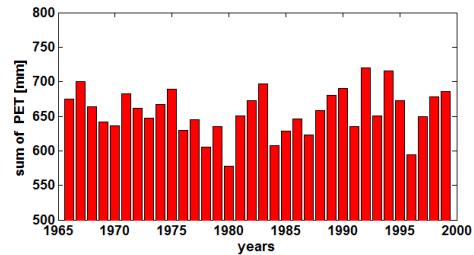
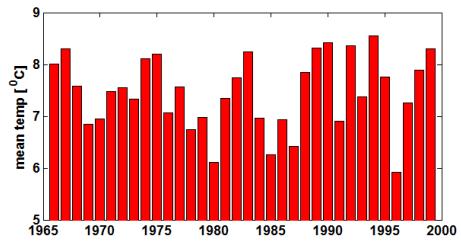
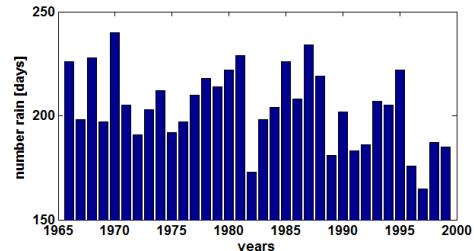
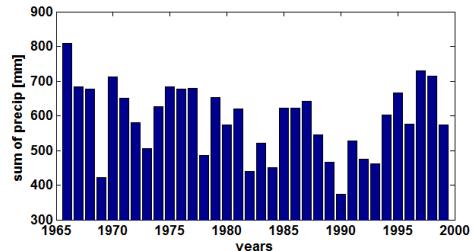


Climatic variables:

- Precipitation
- Air temperature
- Potential evapotranspiration

Statistical descriptors:

- Maximum value
- Mean value
- Median



	min	max	mean
Sum of precip [mm]	374	810	590
Number rain [days]	165	240	204
Mean temp [°C]	5.9	8.6	7.5
Sum of PET [mm]	578	720	656

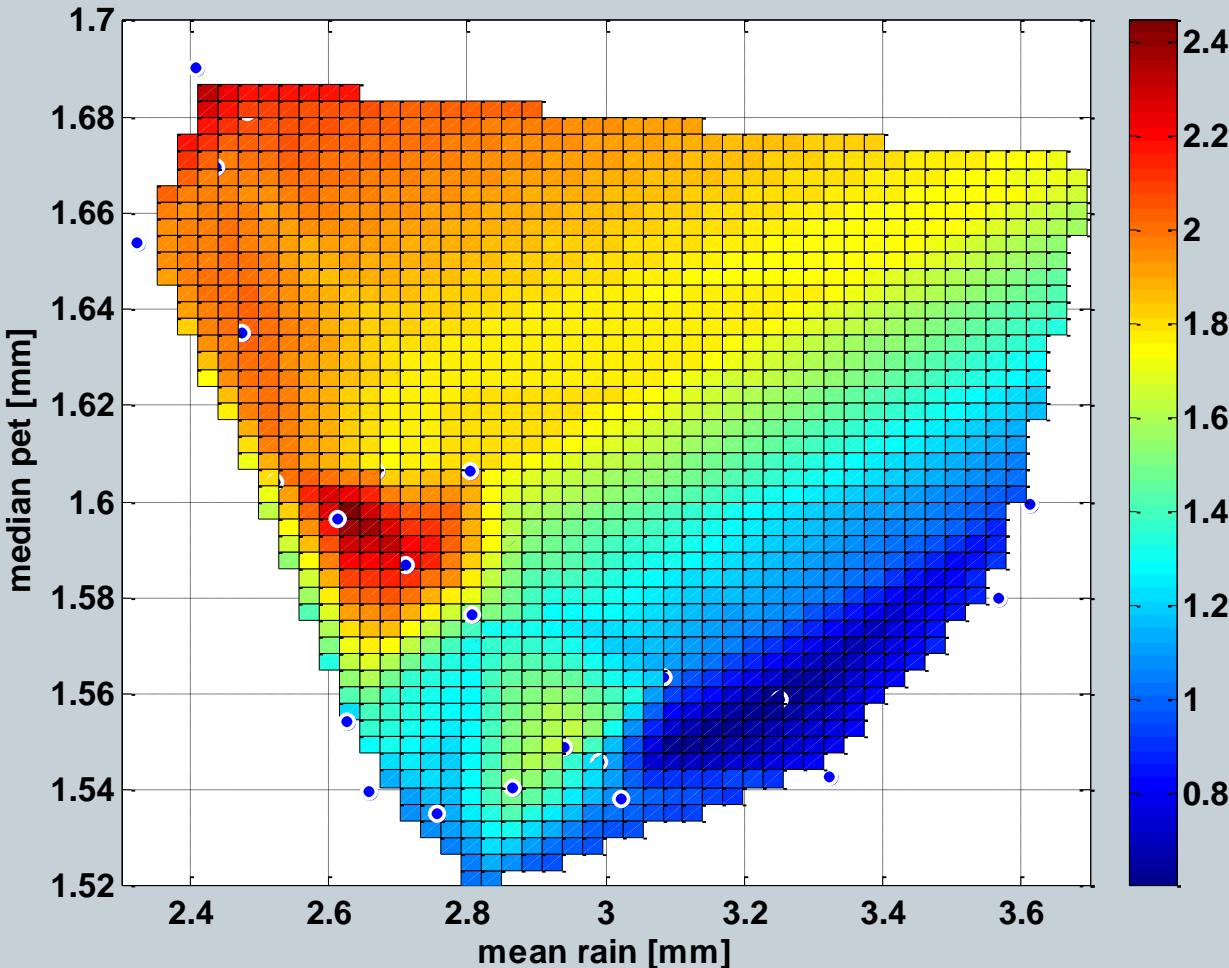
Linear regression

- We developed two regression models

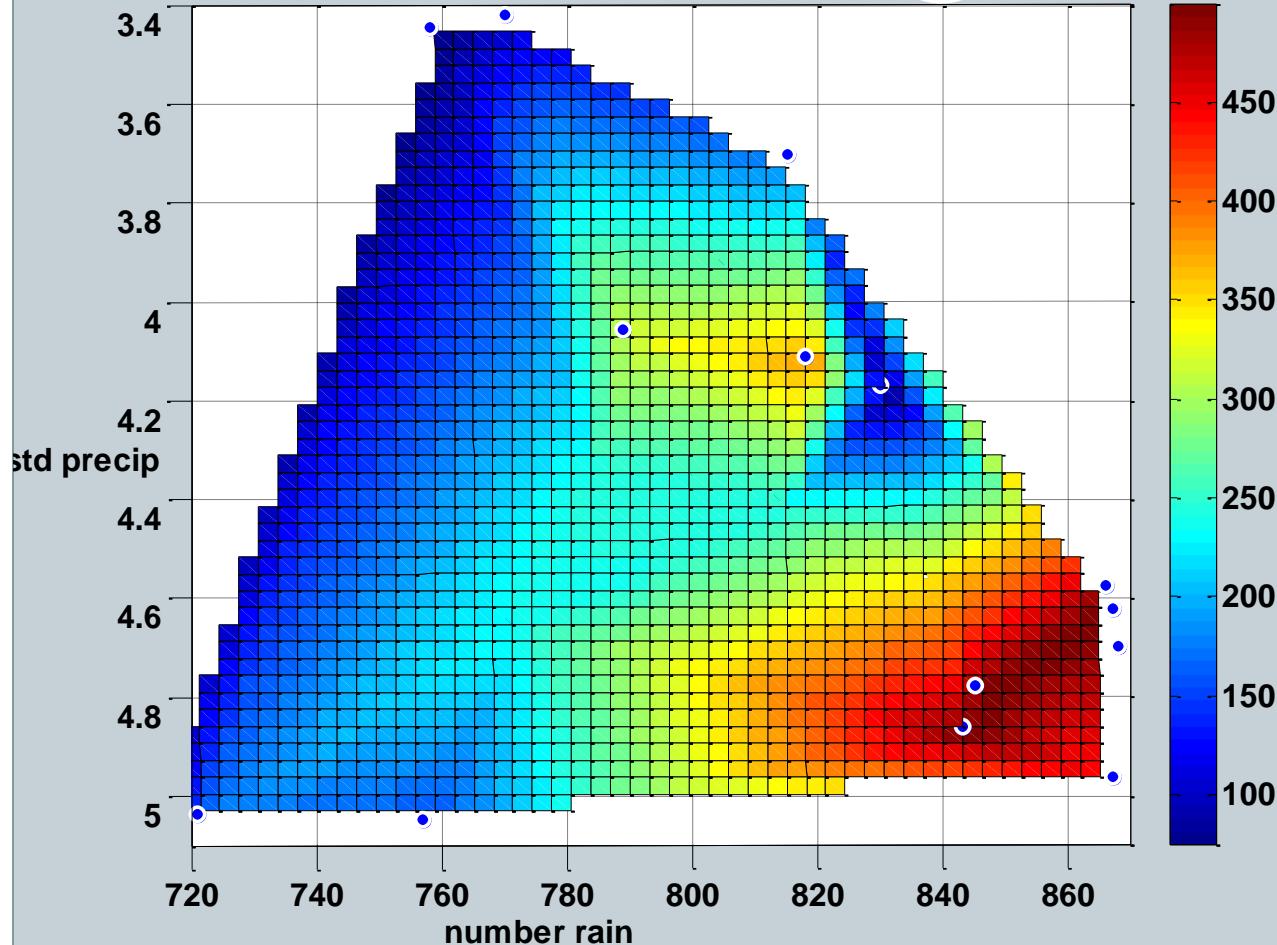
1. For all periods

2. For periods with good results of model calibration
 $NS > 0.5$

All periods		
Param	Climatic indices	R ₂
FC	Max precip, number of days with rainfall	0.6031
KUZ1	Mean temp, max temp	0.4179
PGRAD	Median rainfall, max pet	0.2431
PKORR	Mean rainfall, median rainfall	0.5409
SKORR	Mean precip, median PET	0.7004
NS > 0.5		
Param	Climatic indices	R ₂
FC	Std precip, number of days with rainfall	0.7392
KUZ1	number of days with rainfall, max temp	0.5080
PGRAD	Median rain, max pet	0.3482
PKORR	Mean rain, median rain	0.4782
SKORR	Mean precip, median PET	0.6010



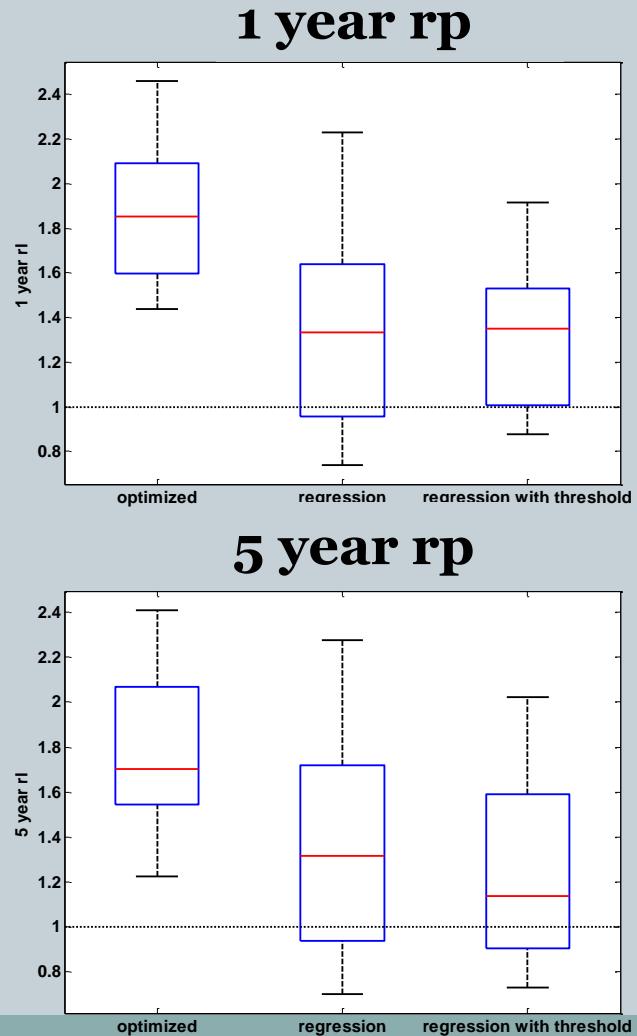
- $\text{SKORR} = f(\text{mean rain}, \text{median PET})$
- Blue dots represent estimated points (31 points-all periods)
- SKORR values are positively correlated with median PET and negatively correlated with mean rainfall



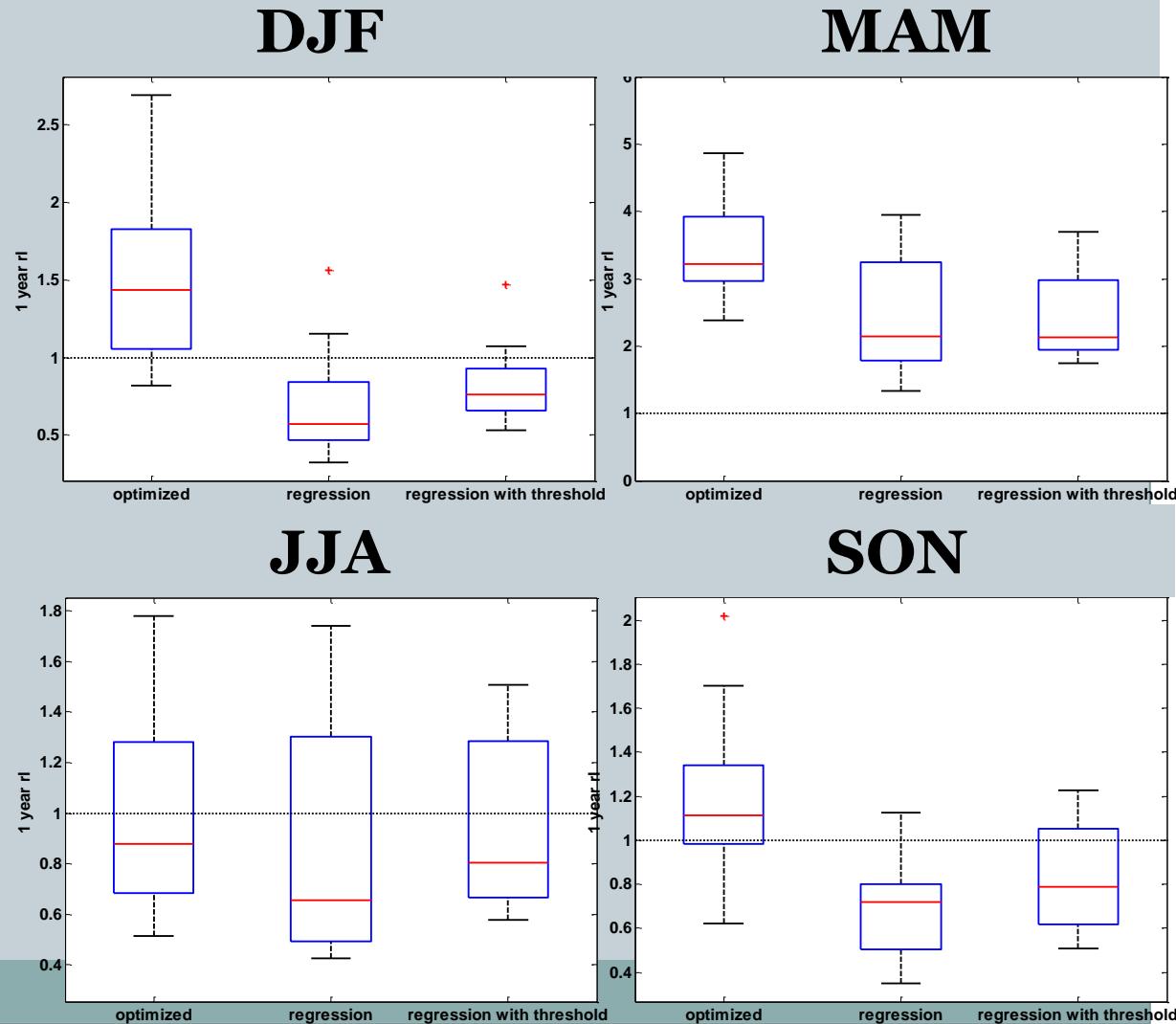
- $FC=f(\text{number rain, std precip})$
- FC value depends mostly on std of precip and number of days with rainfall
- The higher std of precip and number of days with rainfall the larger the FC value

- 15 RCM/GCM with Emission scenario A1B provided in the framework COST FloodFreq
 - Reference period -1961-1990
 - Future period – 2071-2100
- Bias correction - Empirical Quantile Mapping provided in the framework COST FloodFreq
- Hydrological projections:
 - Stationary conditions - one parameter set optimized for complete period
 - Nonstationary conditions - parameters estimated by linear regression for all periods
 - Nonstationary conditions - parameters estimated by linear regression for periods with $NS > 0.5$
- Flood quantile – POT method, the software provided in the framework COST FloodFreq

- A comparison of **relative changes in flood quantiles (sim/obs): 1 and 5 year rp** estimated for simulated versus observed time series
- Application of regression models leads to better estimates of median from RCM/GCM ensemble
- Second regression model gives smaller variability of projected changes between RCM/GCMs



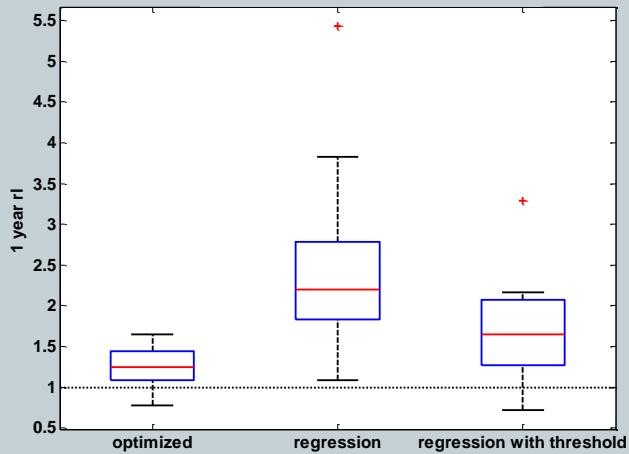
- **Seasonal changes** in flood quantiles derived based on simulated vs observed time series 1 year rp
- **Similar tendency** of changes between methods is estimated **for spring (MAM) and summer (JJA)**
- **Differences** for **winter (DJF) and autumn (SON)**



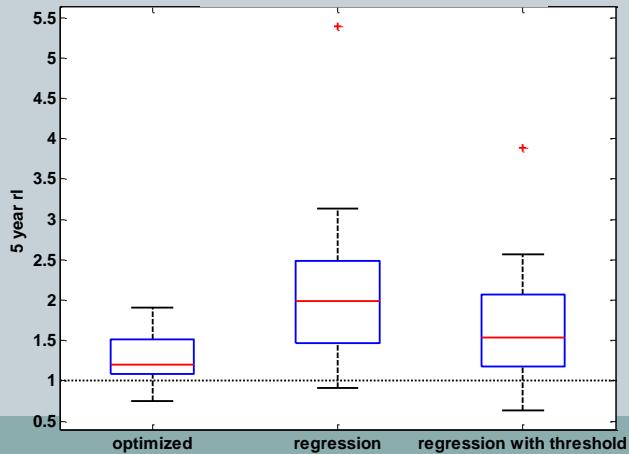
- Analysis of **changes in flood quantiles 1 and 5 year rl** between future and reference periods
- Similar tendency of changes – an increase of flood quantiles 1 and 5 year rl
- Applications of regression models lead to higher changes in flood peaks
- Regression with threshold ($NS > 0.5$) gives smaller variability of projected changes in flood quantiles compared to regression without threshold



1 year rl

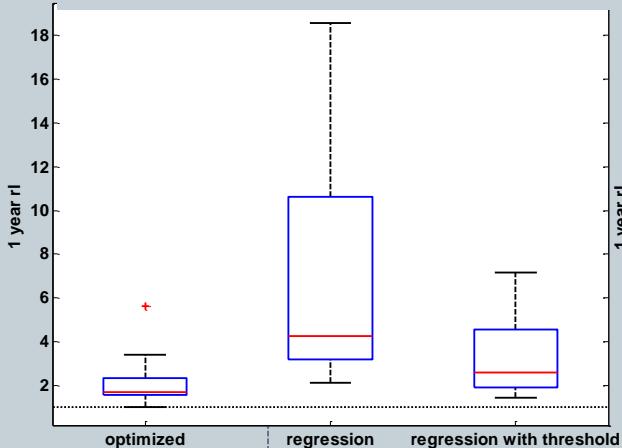


5 year rl

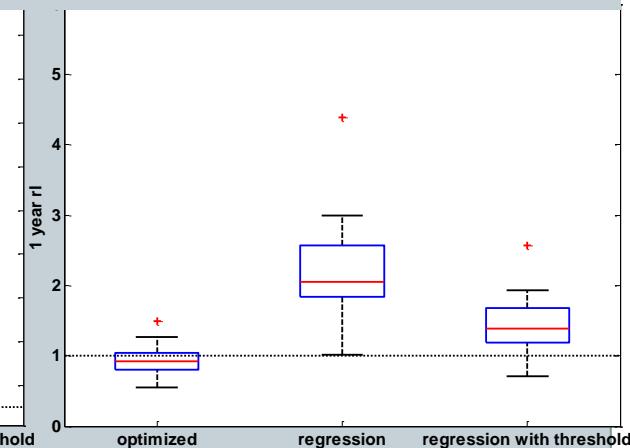


- **Seasonal changes in flood quantiles, 1 year rl**
- Similar tendency of changes is estimated for winter and autumn
- Differences between methods for spring (MAM) and summer (JJA) seasons
- A very large variation of changes in winter (DJF) and autumn (SON) for regression model without threshold

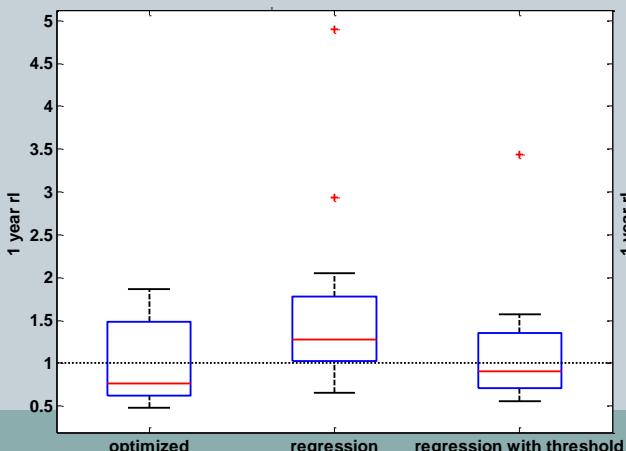
DJF



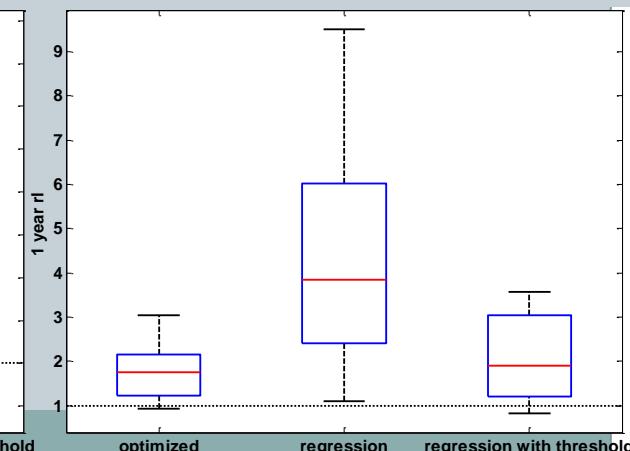
MAM



JJA



SON



Summary

- We have presented an assessment of the impact of climate change on flood quantiles taking into account dependence of HBV model parameters on climate characteristics.
- We derived two regression models for 5 parameters that have the largest impact on the value of the objective function (NS).
- Parameters of HBV model depend on: number of days with rainfall, mean rainfall, mean temp and median PET.
- Analysis of flood quantiles estimated for simulated and observed time series indicates that regression models give better estimates.
- Comparison of changes in flood quantiles between changed climate and reference periods indicates that application of regression models results in potentially larger changes.